



Dual-Phase Inorganic Membrane for High Temperature CO₂ Separation

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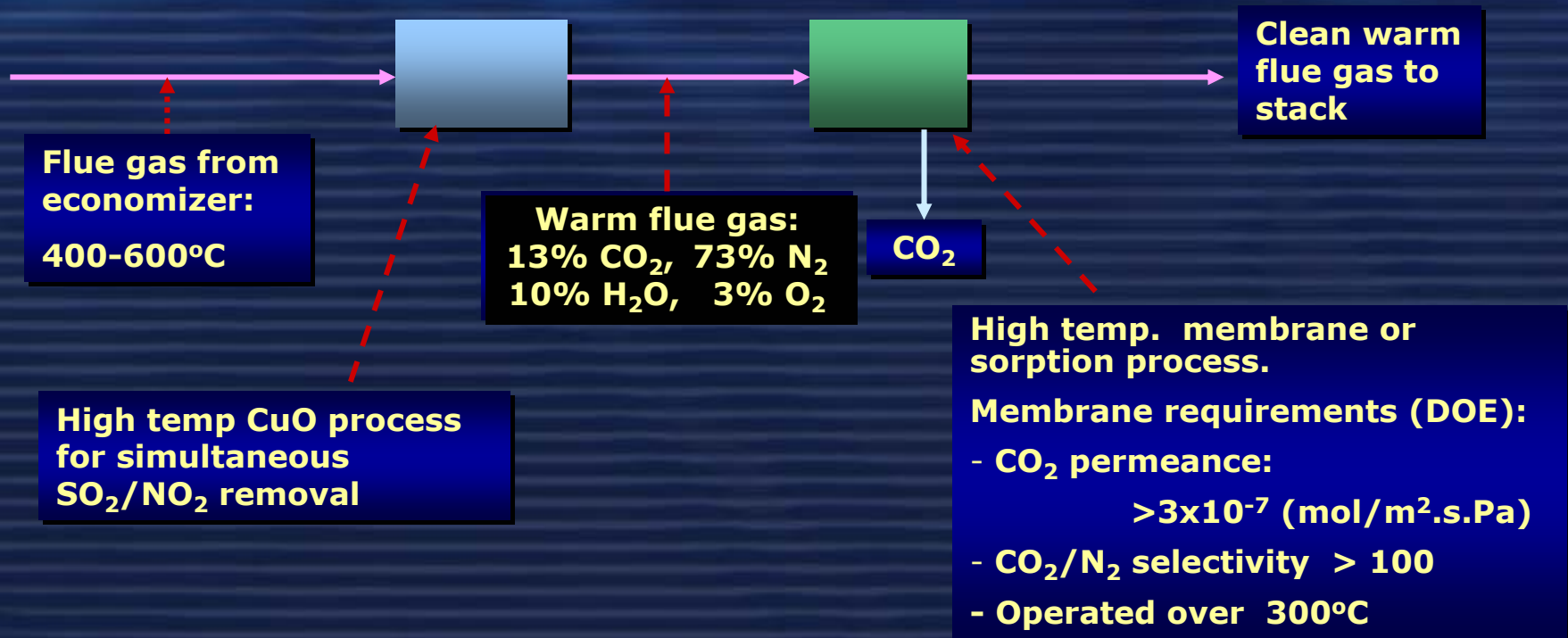
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Motivation

- ***Why do we need to separate CO₂?***
 - Carbon dioxide emits from most industrial facilities
 - Carbon dioxide causes 'Green House effect'
 - Possible use as a feedstock (warm CO₂) to synthesize fuels
- ***Why do we use membrane for CO₂ separation?***
 - Simple, continuous and energy efficient process
 - Applicable to the process at high temperature

Impact of this research



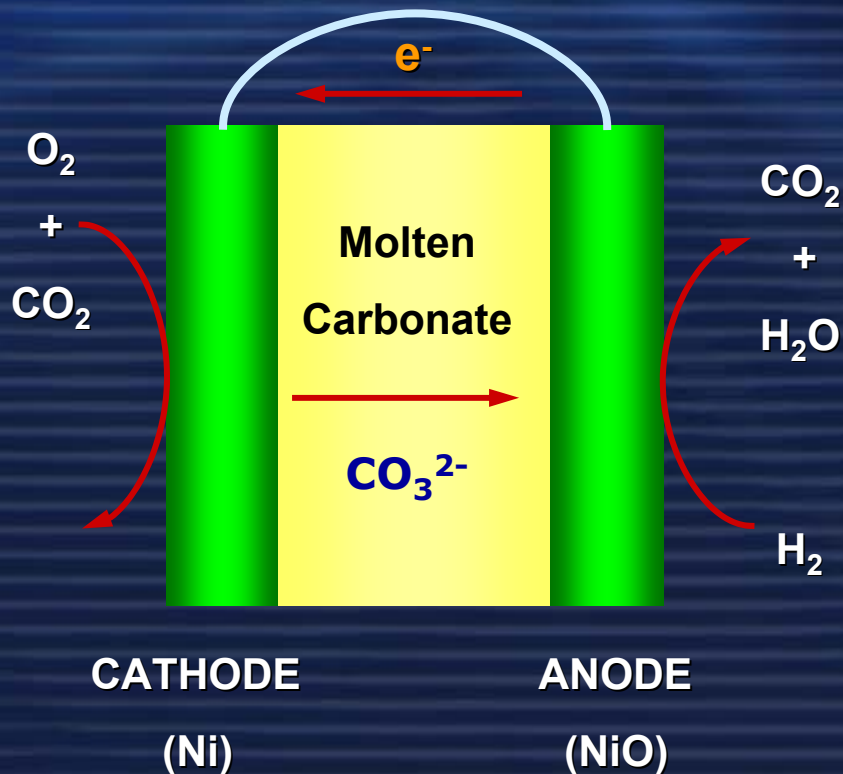


Inorganic membrane for CO₂ separation

- Polymeric membrane (unstable at high temperature)
- Microporous inorganic membrane (low selectivity at $T > 350^{\circ}\text{C}$)
- Ionic conducting membrane (from concept of fuel cell):

Operated at $400\text{--}600^{\circ}\text{C}$ with high selectivity

Principle of MCFC



Common electrolyte :

Eutectic composition of Li_2CO_3 / K_2CO_3 (62 mol% / 38 mol%)

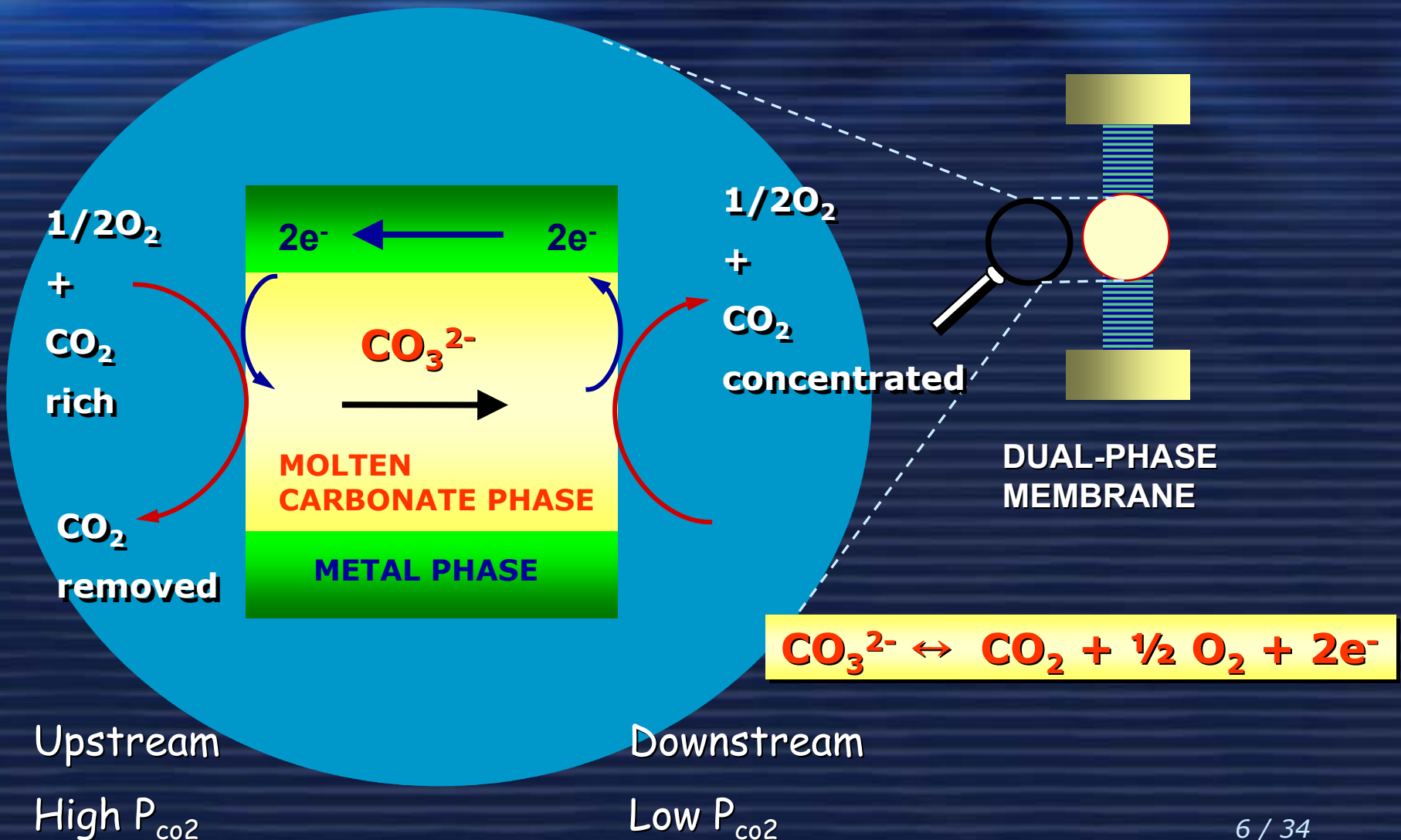
Operating Temperature :

600 ~ 650°C

Major problem :

Precipitation / Contamination of electrodes, reducing performance

Concept of dual-phase membrane





Objectives

- **Synthesis of the dual-phase membrane**
 - Prepare dense and stable dual-phase membrane
- **Characterization of dual-phase membrane**
 - Gas-tightness for He and N₂
 - XRD / SEM analysis → Identification of dual phase
- **Design of high temperature seal & cell**
 - Sealing Test with various seals → Gas tight cell design
- **CO₂ separation at high temperature**
 - Permselectivity of CO₂/N₂ (400-600°C) > 100
 - Permeance of CO₂ (400~600°C) > 1~5 x10⁻⁷ mol/m².s.Pa



Experimental Strategy

- **Development of methods for membrane preparation (Completed)**
 - Material selection, contact time, temperature, preheating
- **Membrane characterization (Completed)**
 - He gas tightness / XRD / SEM with EDS
- **Designing of high temperature seal and cell (Completed)**
 - He permeation and stability test with various seals
- **Single / Binary gas permeation test (Completed)**
 - gas (He, CO₂, N₂, O₂+CO₂) permeances at various Temp.
- **Separation with multi-component gas (continued)**
 - Multicomponent separation system (CO₂, N₂, O₂ mixture)

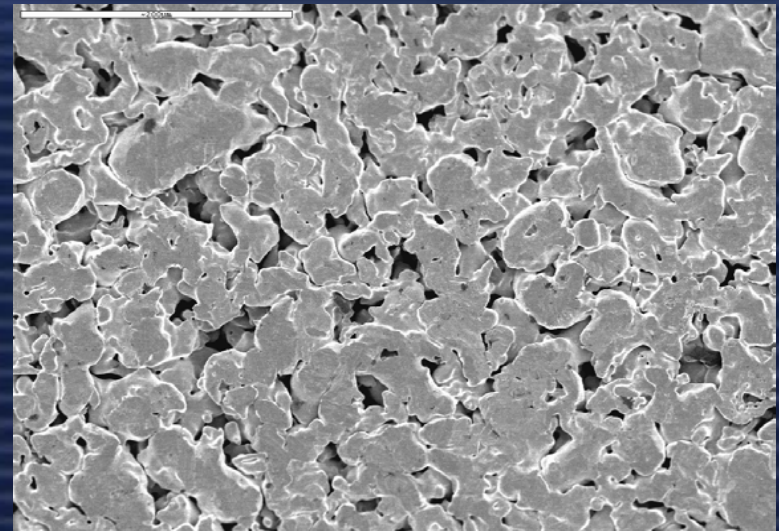
Material Selection

Metal support

General information

Material	Stainless steel 316
Structure	Spherical particle compacted
Media Grade	0.5, 2, 5, 10
Porosity	25-45%
Pore diameter	1~10μm
Electrical Conductivity	10⁴ S/cm

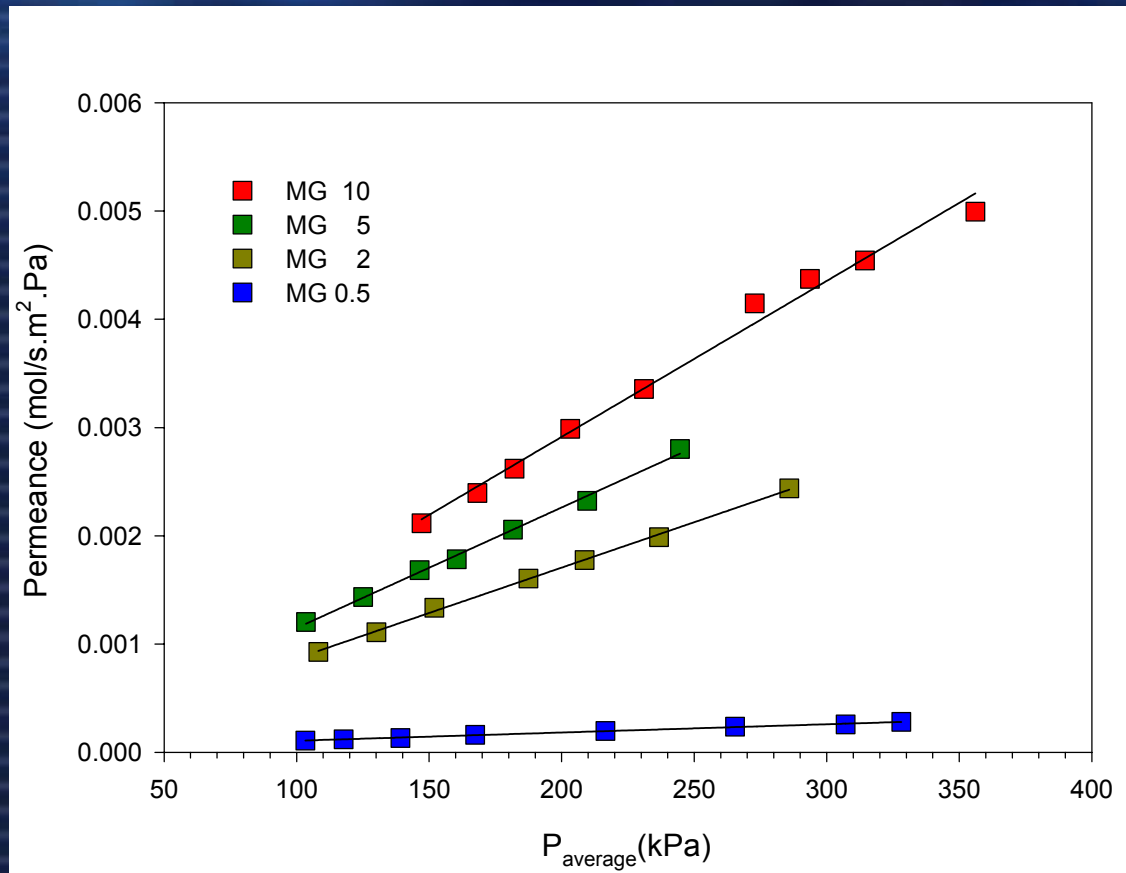
Media Grade 0.5 (SEM, 200x)



➤ He permeation test → Selection of suitable support



Characterization of metal substrate



He Permeance vs Average Pressure



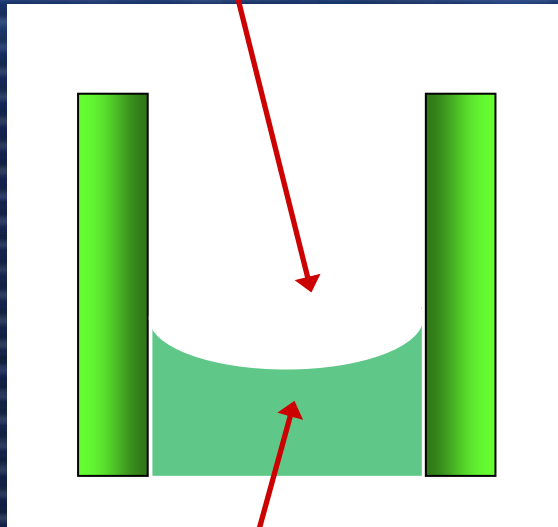
Characterization of metal substrate

Parameters related to pore size with various supports

Media grade	$b \times 10^{-10}$	$a \times 10^{-5}$	$b/a \times 10^{-5}$	$r_p [\mu\text{m}]$	τ	Average pore diameter $[\mu\text{m}]$
0.5	7.44	3.64	2.05	2.65	3.93	5.30
2	83.84	2.96	28.34	36.75	93.71	73.50
5	111.37	3.45	32.25	41.82	99.22	83.64
10	144.07	3.25	44.34	57.51	152.64	115.02

Molten carbonate infiltration

Metal substrate pore



Molten carbonate

$$\Delta P \equiv \frac{2\sigma}{R}, r \equiv R \cos \theta$$

$$r \equiv \frac{2\sigma \cos \theta}{\Delta P}$$

where,

$$\sigma = 237 \text{ mN/m}^2$$

$\theta = 0$ for stainless steel

Capillary pressure $\Delta P = 1 \text{ atm}$



Substrate pore size $9 \mu\text{m}$.

Media grade 0.5 was chosen



Material Selection

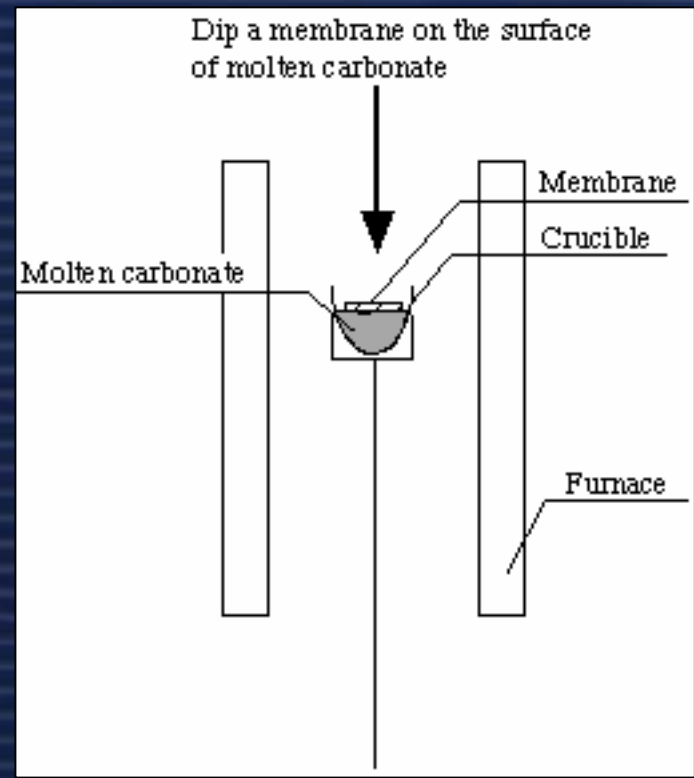
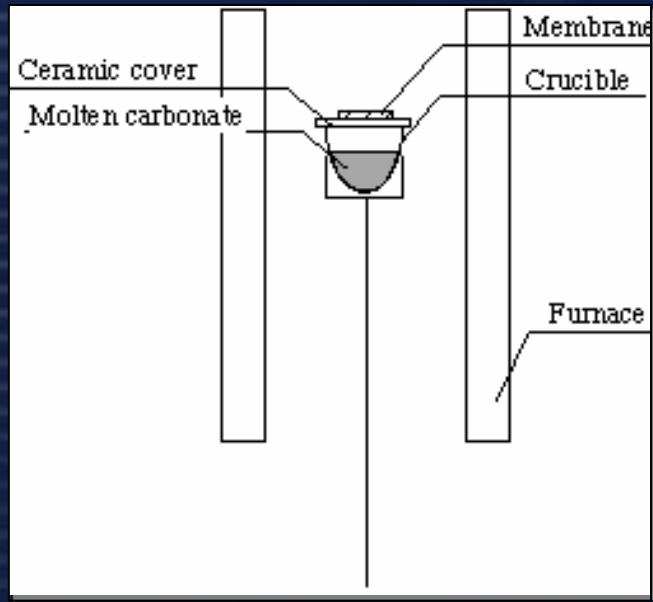
Carbonate Mixture

	Li/Na/K Carbonate	Li/K Carbonate	Li/Na Carbonate	Na/K Carbonate
Composition (mol%)	43.5/31.5/25	62/38	52/48	56/44
Melting Point (°C)	397	488	501	710
conductivity (S/cm)	1.24	1.15	1.75	1.17

- Low melting point and high electrical conductivity
→ Li/Na/K (43.5/31.5/25 mol%) was chosen

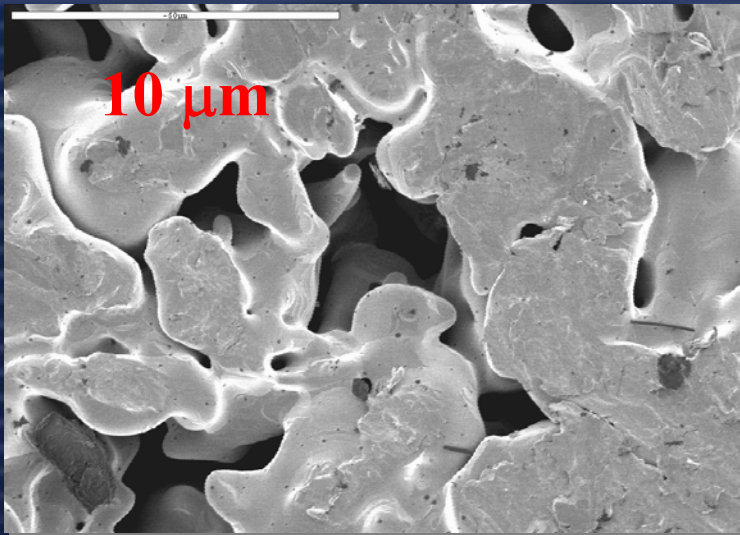
Preparation of the dual phase membrane

- Mix and melt Li/Na/K carbonate (43.5/31.5/25 mole%)
- Infiltrate molten carbonate into the pores by dipping method.



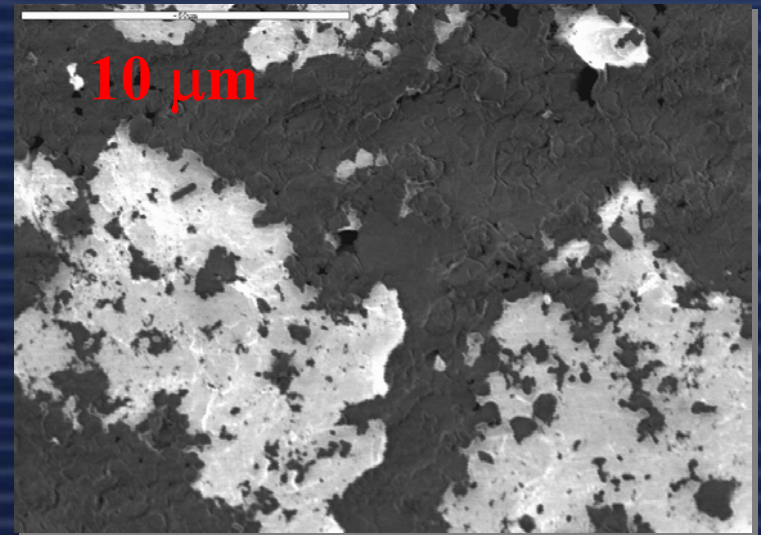
SEM image of dual-phase membrane

- **Before infiltration**



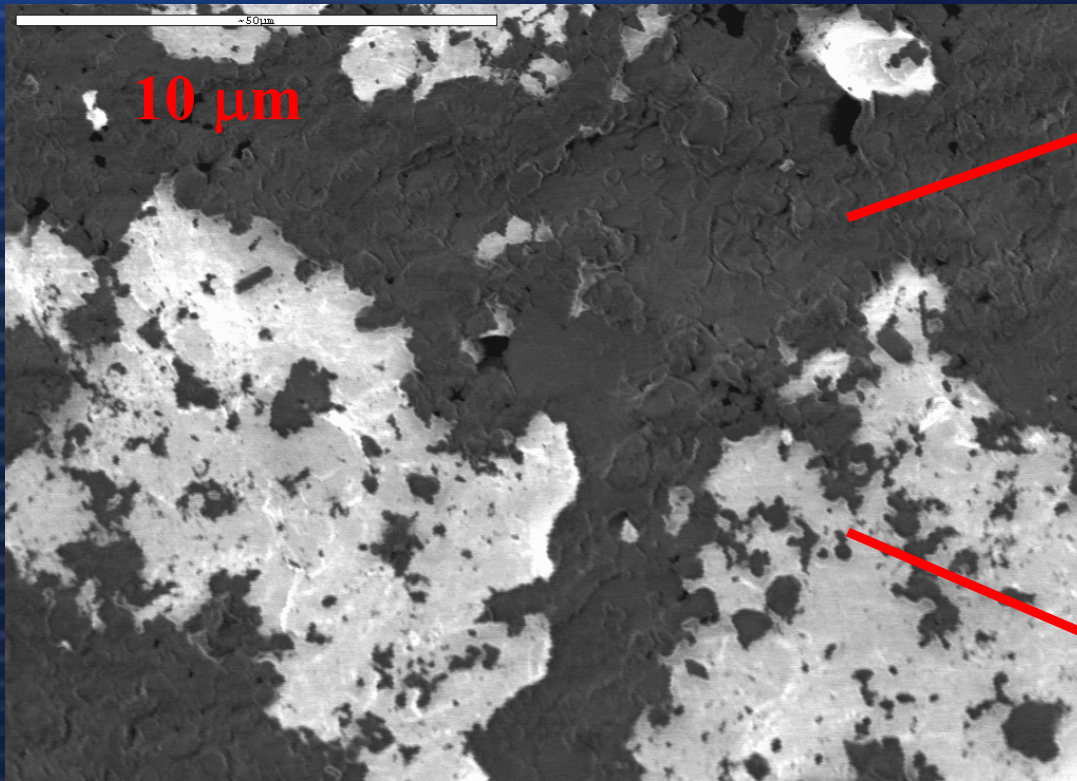
Metal support, 1000x

- **After infiltration**

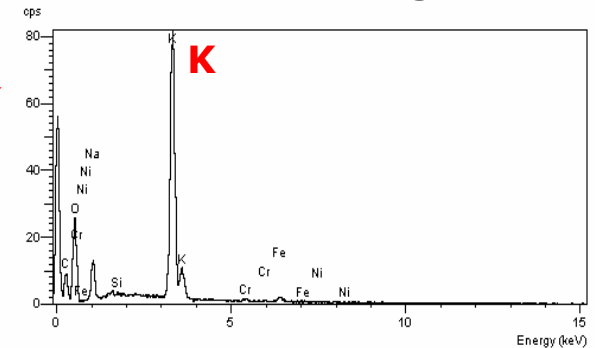


Metal-carbonate, 1000x

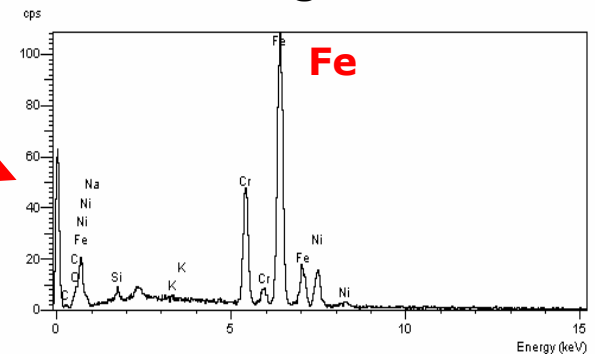
Identification of dual-phase structure



Carbonate rich region

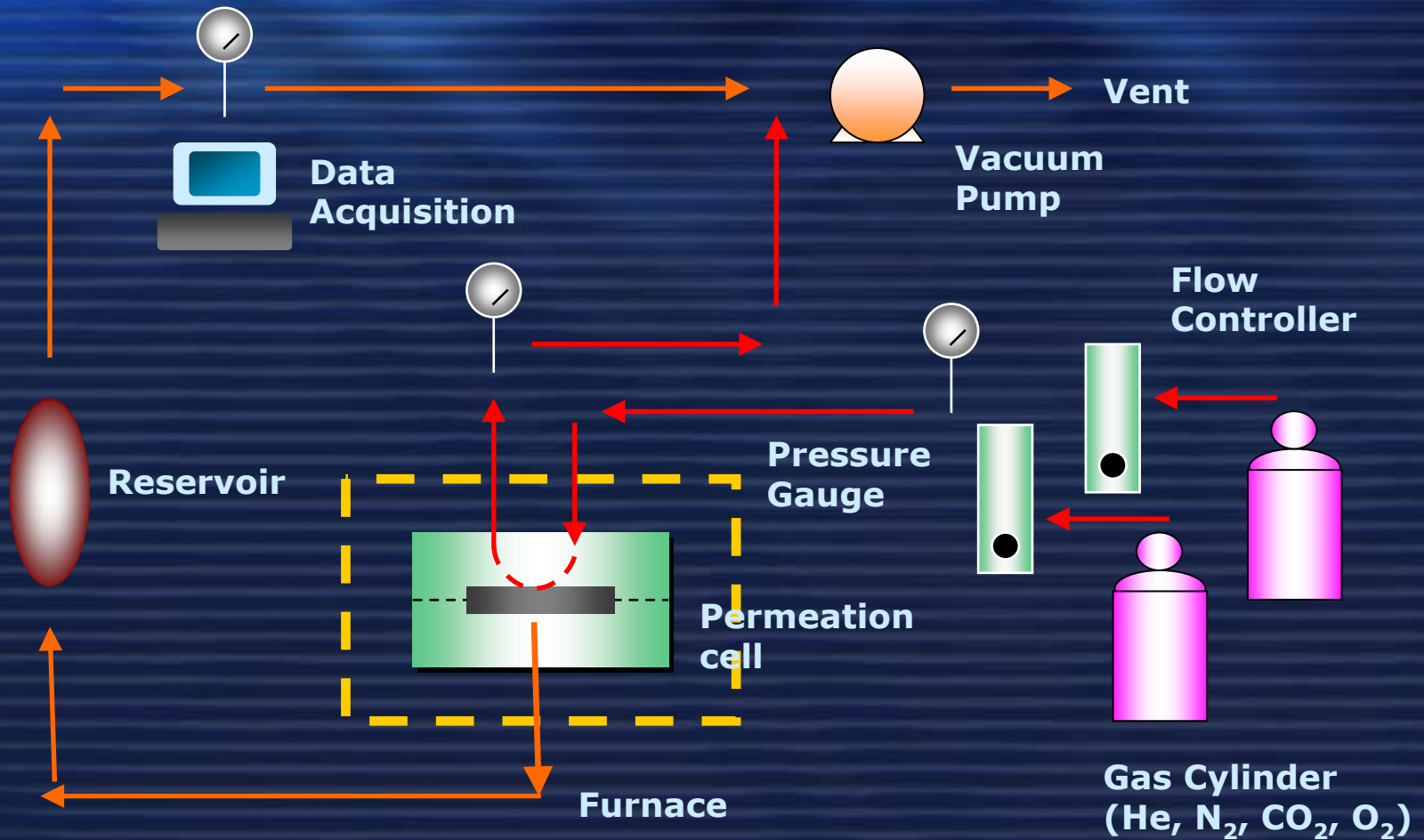


Metal rich region



➤ Dual-phase membrane is successfully prepared

Experimental Apparatus



unsteady state type Gas permeation setup



Seal design for high temperature

Comparison chart for high temperature seals

Seal	Rubber	Pure Graphite	Graphite Composite	Nickel Alloy	Gold
He Permeance (mol/s.m².Pa) at R.T.	2×10^{-10}	1×10^{-7}	8×10^{-9}	7×10^{-9}	6×10^{-10}
He Permeance (mol/s.m².Pa) at 450°C	-	3×10^{-7}	3×10^{-9}	7×10^{-9}	3×10^{-10}
Stability at high Temp.	Burn	Vaporization	Vaporization	inert	Inert

Theoretical permeation flux

- Wagner Theory**

$$J(CO_2) = - \frac{RT}{16 F^2 L} \int_{\ln P_{CO_2}}^{\ln P'_{CO_2}} \frac{\sigma_{el} \sigma_{ion}}{\sigma_{el} + \sigma_{ion}} d \ln P_{CO_2}$$

F (Faraday constant) : 9.65×10^4 C/mol , R (Gas constant), d (Thickness)

$$J(CO_2) \propto \frac{\sigma_{el} \sigma_{ion}}{\sigma_{el} + \sigma_{ion}} \cong \sigma_{ion} \left(\because \sigma_{el} \gg \sigma_{ion} \right)$$

σ_{ion} (CO_3^{2-} conductivity) : 0.5-2 S/cm (at 600 °C, $P_{CO_2} = 1/3$ atm)

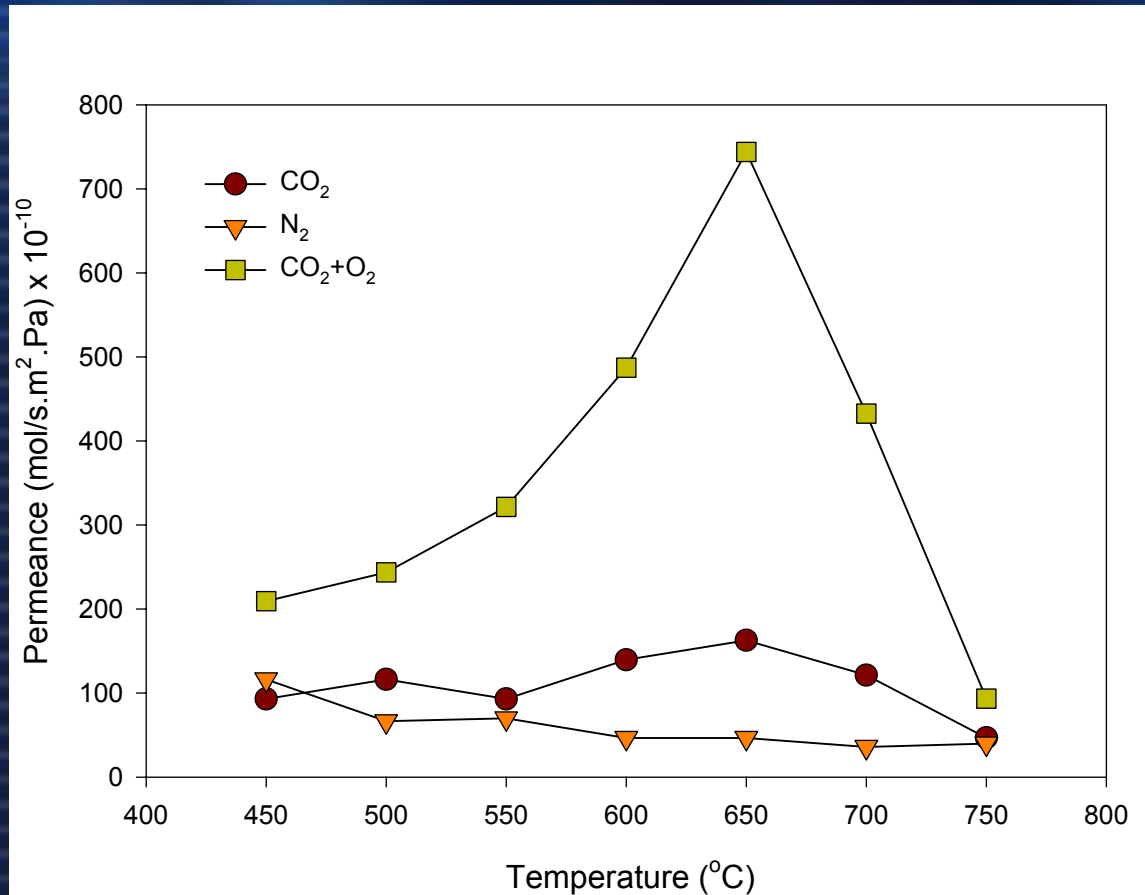
σ_{el} (Electronic conductivity) : 10^4 S/cm

Rate determining variable : σ_{ion}

CO_2 permeance : $2 \sim 10 \times 10^{-7}$ mol/m².s.Pa (for 1 mm thick membrane)

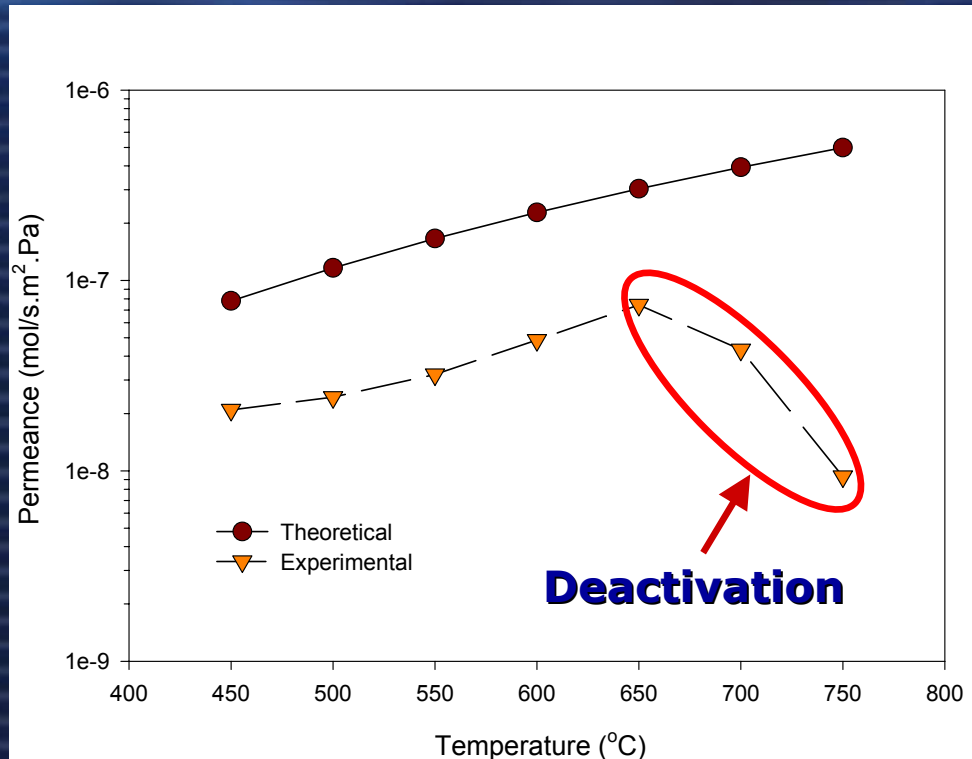


Single / Binary gas permeation test



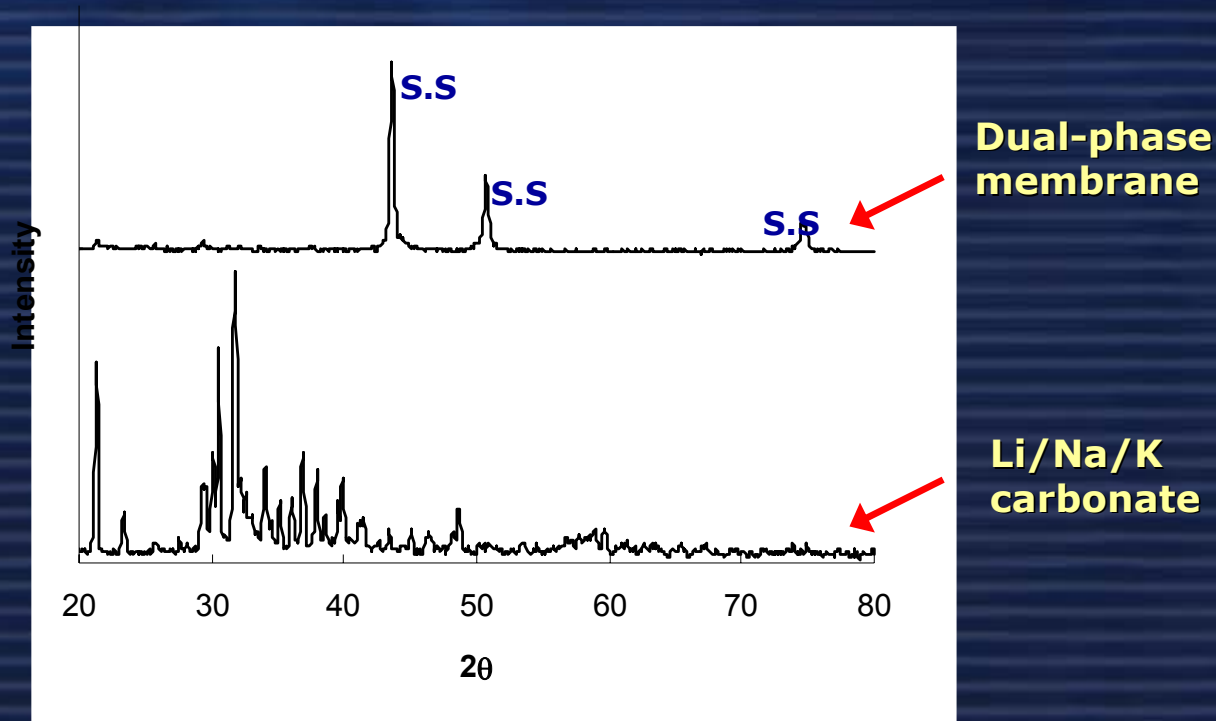
Gas permeation at various temperature (450-750°C)

Comparison of permeation flux



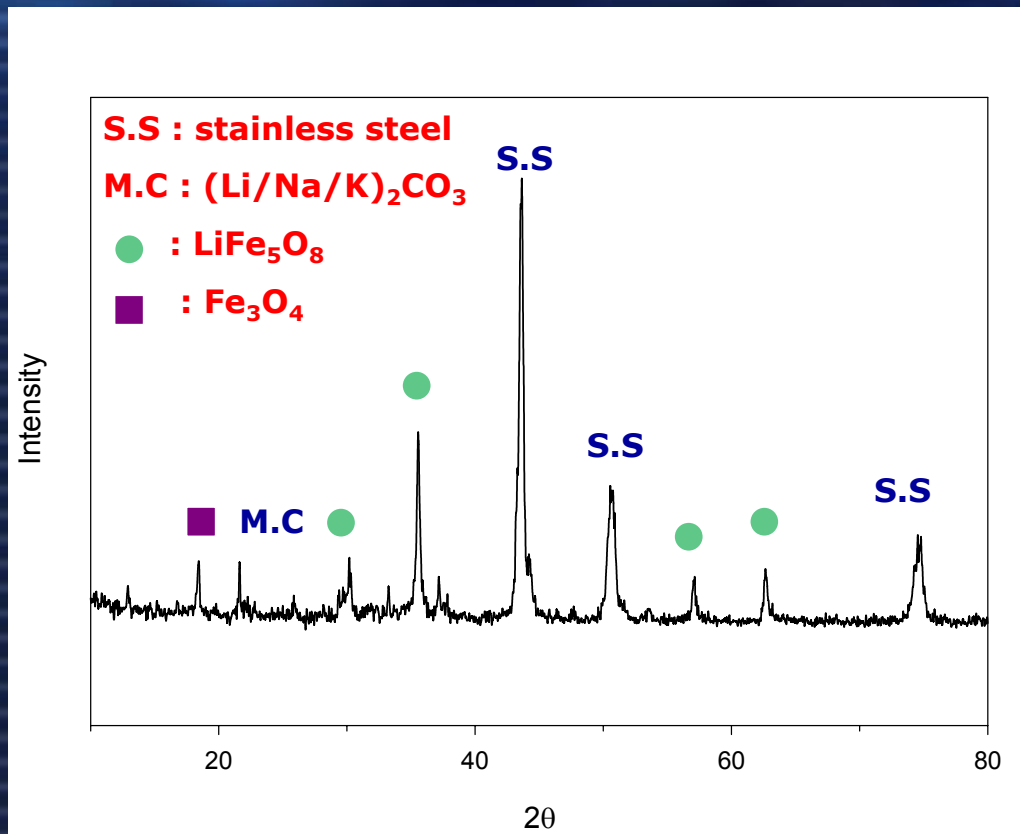
Deactivation occurred at higher than 650°C,

Structure of metal-carbonate membrane



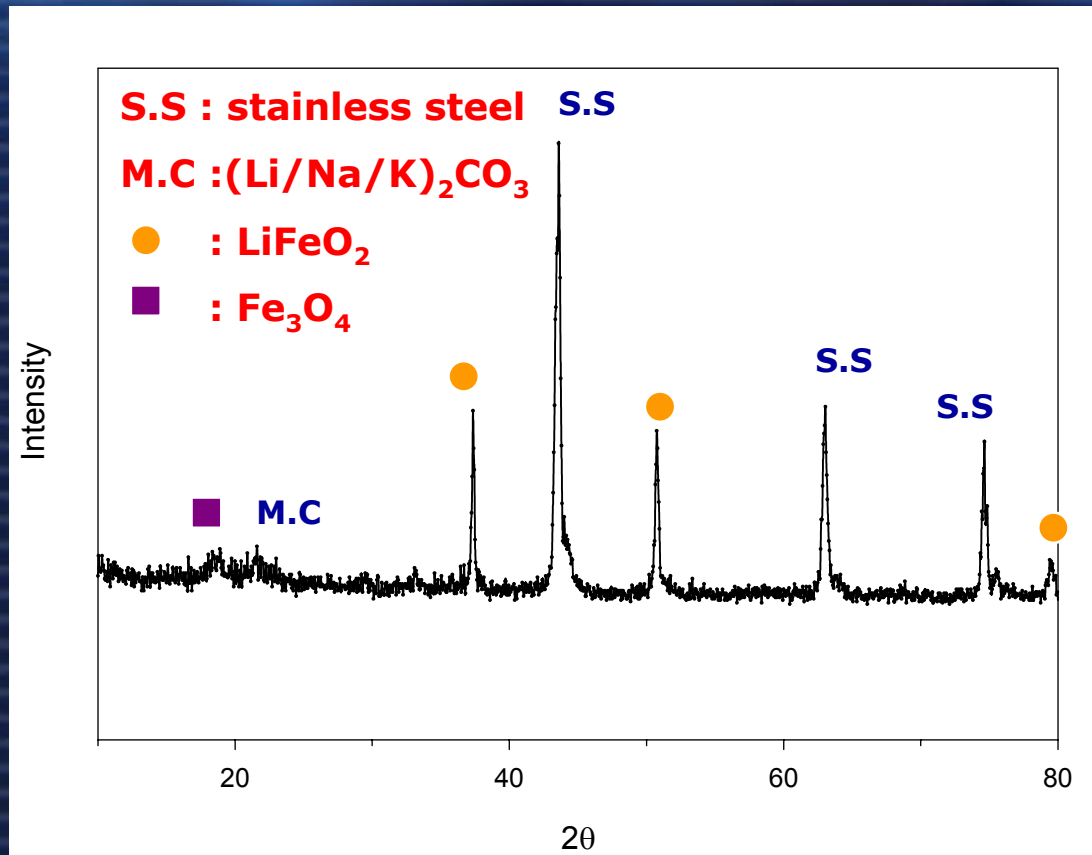
**XRD pattern of dual-phase membrane
& molten carbonate**

XRD analysis after permeation



XRD pattern of membrane after CO_2 permeation at 500°C

XRD analysis after permeation



XRD pattern of membrane after CO₂ + O₂ permeation at 600°C



Accomplishments

- Dense and stable dual-phase metal-carbonate membranes were successfully prepared by direct infiltration method. He gas-tightness of dual-phase membrane was 10^{-6} times higher than that of metal support.
- Permeance of CO_2 with O_2 increases with temperature and reaches the optimum at 650°C . Maximum ratio of CO_2/N_2 permeance was about 16 and CO_2 permeance was $7 \times 10^{-8} \text{ mol/s.m}^2.\text{Pa}$.
- At higher temperature, membrane was deactivated due to oxidation, causing a significant decrease in permeance of CO_2 with O_2 . XRD results shows that Iron oxide was formed on the membrane after CO_2 with O_2 permeation experiment .



Future work

- **Ceramic-carbonate system for CO₂ separation**
 - Deactivation of metal carbonate membrane is caused by oxidation of support or reaction of metal support with molten carbonate.
 - Perovskite type ceramic support (Lanthanum Cobaltite) is an alternative support with better oxidation resistance than metal and good electronic conductivity.
- **Multi-component separation experiment**
 - Design and setup new separation/permeation setup
 - Perform separation of CO₂ from mixture of N₂, CO₂, O₂



Alternative support

Porous ceramic support

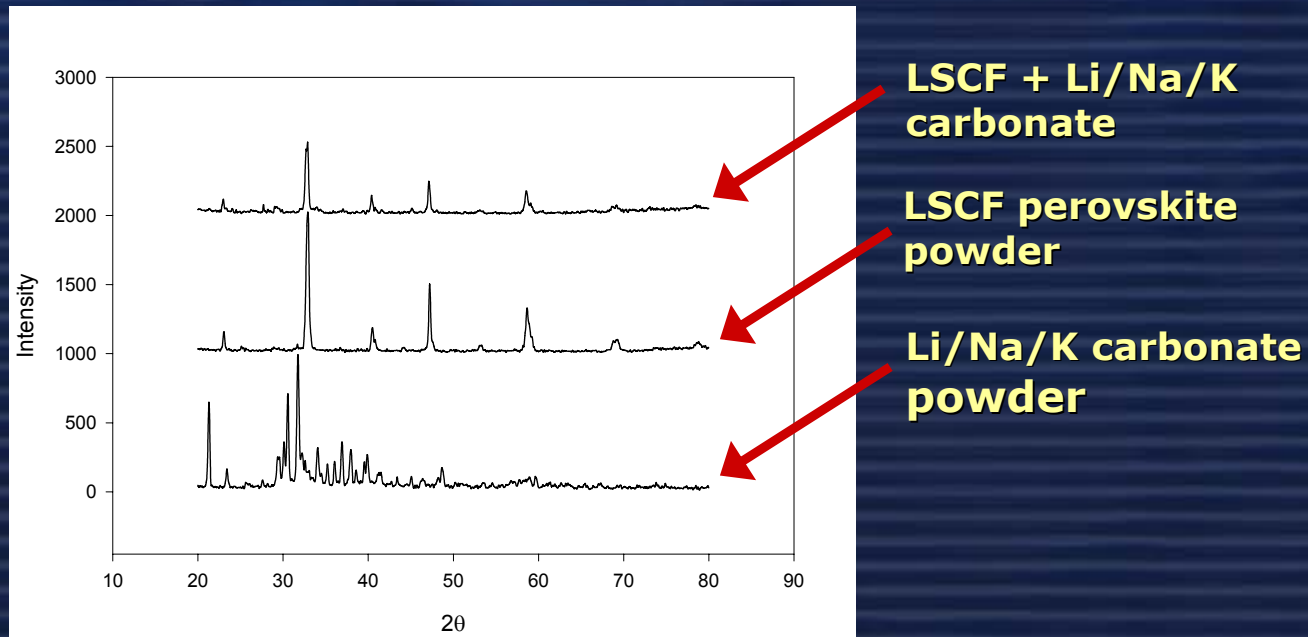
Material	Lanthanum Cobaltite
Composition	$\text{La}_a\text{Sr}_b\text{Co}_c\text{Fe}_d\text{O}$ $a:b:c:d=6:4:8:2$
Electrical Conductivity	1200-1500 S/cm (400-600°C)
Preparation Method	Citrate Method



Preparation of ceramic supports

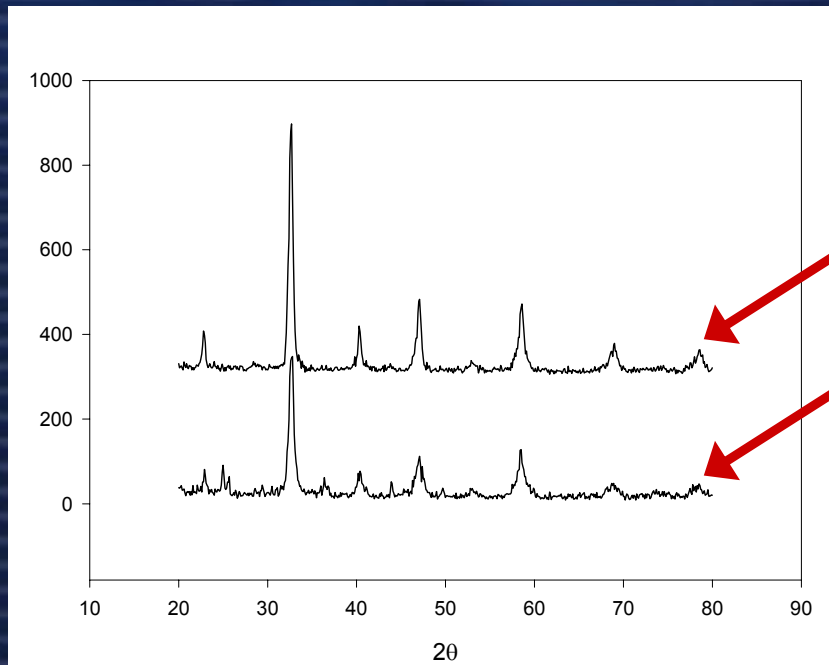
Step	Details
Precursors	$\text{La}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$, $\text{Sr}(\text{NO}_3)_2$, $\text{Fe}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$, $\text{Co}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$
Polymerization	100-105°C, stirring, 5h
Vaporization	100-105°C, 5h
Powder Drying	110°C
Self Ignition Step	400°C, 1hr
Preliminary Sintering	600°C, 5-24hr
Final Sintering	900°C, 20hr, Ramping Rate 2° C/min

Reactivity of LSCF + carbonate mixture



**XRD peaks of LSCF + Carbonate mixture
(600°C, overnight)**

Electronic conduction of the support



Before & After Final sintering 900°C, 24h

Electron-
conductive

After final sintering at
900°C

Before final sintering at
900°C (sintered 600°C)

not
Conductive



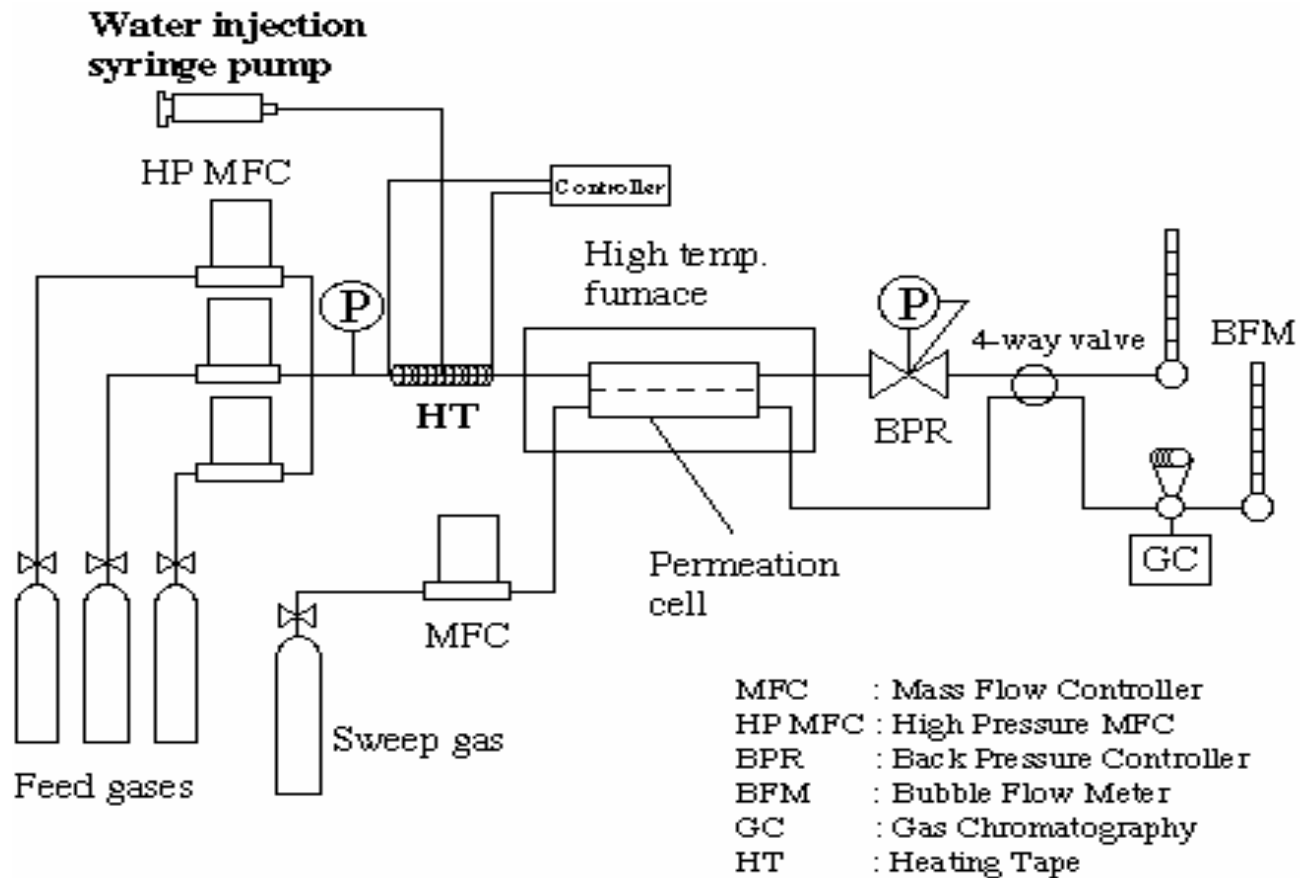
Comparison of support

Support	Porous 316LSS (Grade 0.5)	LSCF support	α -Alumina
Permeance (mol/s.m ² .Pa)	1.0×10^{-4}	1.1×10^{-5}	8.0×10^{-6}
Mean pore size (μm)	5.8	2.2	1.0

- Variables to control pore size distribution →
Particle size, Sintering temperature



Multicomponent separation system





Thank you for your attention



(cont'd)

**Permeance of CO₂, N₂, O₂+CO₂ and their selectivity
at 450-700 °C**

Temp. (°C)	Permeance (mol/s.m².Pa) x 10⁻¹⁰			Selectivity	
	CO₂	N₂	O₂ + CO₂	CO₂ / N₂	O₂ + CO₂ / N₂
450	93.00	116.24	209.24	0.80	1.80
500	116.24	66.44	243.60	1.75	3.67
550	93.00	69.76	321.48	1.33	4.61
600	139.48	46.48	487.16	3.00	10.48
650	162.72	46.48	744.00	3.50	15.98
700	121.28	35.76	432.56	3.39	12.09
750	46.68	39.80	93.36	1.17	2.34